

## · 基础研究 ·

# 不同材料矫形棒在青少年特发性脊柱侧凸矢状面重建中作用的有限元研究

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**【摘要】目的** 探讨不同材料、不同预弯弧度矫形棒在青少年特发性脊柱侧凸(AIS)矢状面重建中的作用。**方法** 建立从T<sub>1</sub>到骨盆的AIS非线性有限元仿真模型。在建立的有限元模型上进行模拟手术, 分别设定矫形棒的属性为钛合金和钴铬合金, 比较2种材料在28°预弯弧度时对矢状面重建的效果以及螺钉拔出应力的差异。进一步探讨当预弯弧度为40°时, 钛合金棒对矢状面重建的影响。**结果** 建立了完整的AIS仿真三维有限元模型, 模型包括691 271个单元。其中实体单元、壳单元以及仿真单元计数分别为667 459、62 838和575。在28°预弯弧度下, 钴铬合金比钛合金能够更好地矫正AIS矢状面后凸, 但是钴铬棒组螺钉拔出应力显著增加。当预弯弧度为40°时, 钛合金棒对矢状面后凸矫正效果显著优于预弯弧度为28°时, 同时螺钉拔出应力显著增加。**结论** 采用强度较大的钴铬合金棒及适当加大矫形棒预弯弧度有助于矢状面力线的恢复, 但也会导致螺钉拔出应力增加。

**【关键词】** 青少年; 脊柱侧凸; 钛; 铬合金; 内固定器; 生物力学

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## Role of different material orthopaedic rods in sagittal reconstruction in patients with adolescent idiopathic scoliosis: a finite element study

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**【Abstract】 Objective** To investigate the role of different materials and pre-curvature rods in sagittal reconstruction for adolescent idiopathic scoliosis (AIS). **Methods** Base on the CT images (from T<sub>1</sub> to pelvis) of a 14-year-old female AIS patient, a nonlinear three-dimensional finite element model was established by software Mimics. The finite element model was used to simulate the operation. The orthodontic rods were set with titanium alloy and cobalt-chromium alloy. The effect of the sagittal reconstruction and the difference of screw pull-out stress between the 2 materials were compared at 28° pre-bending curve. The effect of titanium alloy rods on the sagittal reconstruction was also discussed when the pre-bending curve was 40°. **Results** A complete three-dimensional finite element model of AIS simulation was established, which consists of 691 271 units. The number of entity units, shell units and imitated units was 667 459, 62 838 and 575 respectively. Correction of sagittal kyphosis in AIS with cobalt-chromium alloy rod was better than titanium alloy rod at 28° pre-bending curve, but the pull-out stress of cobalt-chromium alloy rod increased significantly. When the pre-bending curve was 40°, the correction effect of titanium alloy rod on sagittal kyphosis was significantly better than that of pre-bending curve being 28°, and the screw pull-out stress increased significantly. **Conclusion** It is helpful to restore the sagittal force line by using cobalt-chromium alloy rod with higher strength and increasing the pre-bending curve of the orthodontic rod properly, but it will also increase the pull-out stress of the screw.

**【Key Words】** Adolescent; Scoliosis; Titanium; Chromium alloys; Internal fixators; Biomechanics

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青少年特发性脊柱侧凸(AIS)矫正率的提高得益于椎弓根螺钉的应用, 这使得AIS在冠状面和横断面上的力线能够很好地重建。全椎弓根螺钉带来强大矫形力的同时, 同样也带来系列相关并发症, 如术后胸椎生理弯曲减小<sup>[1-2]</sup>。近年来, AIS矢状面力线的重建越来越受到外科医师的重视, 因为良好的矢状面平衡与患者生存质量显著相关<sup>[3]</sup>。许多因素均可影响AIS患者术后矢状面平衡, 如融合节段选择<sup>[4]</sup>、医师操作技术水平<sup>[5]</sup>和术前矢状面参数<sup>[6]</sup>。对于胸椎结构性侧凸的患者, 胸椎生理弯曲较正常人群要小, 一般<20°, 使术后胸椎生理弯曲不足风险增加。既往研究表明, 矫形棒材料是影响AIS矢状面矫形效果的重要因素<sup>[7]</sup>。本研究通过建立有限元模型, 模拟AIS矫形手术, 探讨不同材料、不同预弯弧度矫形棒在AIS矢状面平衡重建中的作用。

## 1 资料与方法

### 1.1 T<sub>1</sub>至骶骨有限元模型的建立

选择1例AIS患者, 女, 14.3岁, 身高162 cm, 体质量51 kg。术前正位X线片测量T<sub>1~6</sub> Cobb角为24°, T<sub>6~12</sub> Cobb角为48°; 矢状面测量胸椎后凸T<sub>2~12</sub>为

11°, T<sub>10~L<sub>2</sub></sub>为-6°, 腰椎后凸为51°。采用0.8 mm薄层CT扫描T<sub>1</sub>至骶骨, 得到dicom格式图像数据。图像导入Mimics软件(Materialise公司, 比利时), 输出格式为stl的模型数据。将stl数据导入Geomagic Studio软件(Geomagic公司, 美国)对模型进行修补和边界调整。使用SolidWorks软件(SolidWorks公司, 美国)根据上下椎体轮廓构建椎间盘形状, 髓核与纤维环成分比为3:2。仿真模拟前后纵韧带, 根据解剖结构特点构建其余韧带。根据骨质的CT值(亨氏单位, Hu)差异, 使用Mimics软件进行对应赋值, 计算各结构密度( $\rho$ ),  $\rho(\text{kg} \cdot \text{m}^{-3}) = 1.067 \times \text{CT值} + 131$ 。进一步计算各结构弹性模量( $E$ ),  $E=009\ 882 \times \rho^{1.56}$ 。泊松比为0.30。模型中各结构赋值见表1。

荷载与边界条件设定。限制T<sub>1</sub>椎体上终板和骶骨各个方向自由度, 模拟人体直立状态脊柱所受负荷, 最终躯干上身体质量平均施加在每一个节段上。所建立的模型中, 骨组织、终板和韧带分别应用实体单元、壳单元和仿真单元。模型包括691 271个单元, 其中实体单元、壳单元以及仿真单元计数分别为667 459、62 838和575(图1)。

表1 各结构赋值  
Tab. 1 Assignment of different structures

| 属性<br>Property                         | 髓核<br>Nucleus<br>pulposus | 纤维环<br>Annulus<br>fibrosus | 前纵韧带<br>Anterior<br>longitudinal<br>ligament | 后纵韧带<br>Posterior<br>longitudinal<br>ligament | 黄韧带<br>Ligamentum<br>flavum | 棘突间韧带<br>Interspinous<br>ligament | 棘上韧带<br>Supraspinal<br>ligament | 横突间韧带<br>Intertransverse<br>ligament | 关节囊韧带<br>Articular<br>capsule<br>ligament |
|--|---------------------------|----------------------------|--|---|-----------------------------|-----------------------------------|---------------------------------|--------------------------------------|---|
| $\rho/(\text{kg} \cdot \text{m}^{-3})$ | 1.0                       | 1.2                        | 1.1  | 1.1   | 0.9                         | 1.1                               | 1.1                             | 1.1                                  | 1.1                                       |
| 杨氏模量/MPa<br>Young's modulus/MPa        | 1.00                      | 4.50                       | 11.30  | 9.26  | 5.70                        | 4.62                              | 8.58                            | 11.70                                | 22.80                                     |
| 泊松比<br>Poisson ratio                   | 0.49                      | 0.45                       | 0.45   | 0.45  | 0.45                        | 0.45                              | 0.45                            | 0.45                                 | 0.45                                      |

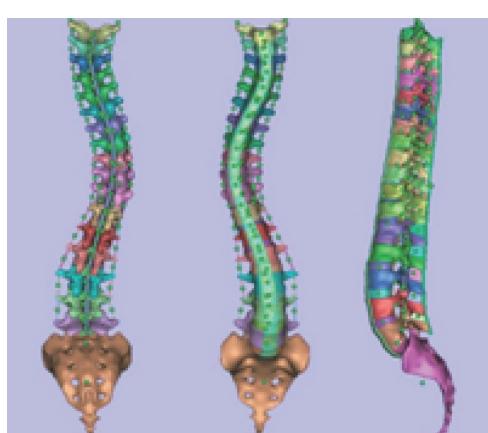
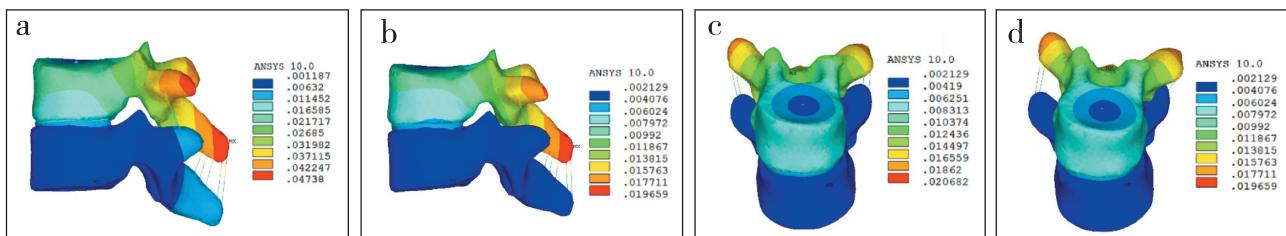


图1 AIS有限元模型  
Fig. 1 Finite element model of AIS

构建的有限元模型与AIS患者术前X线片具有良好的几何相似性, Wilcoxon检验提示椎体各重心到骶骨中垂线距离一致。前屈、后伸、左旋和右旋加载实验表明, 本研究建立的AIS模型与Panjabi等<sup>[8]</sup>的报道一致。本模型采用实物加载, 与既往建立的模型<sup>[9]</sup>相比更接近实体力学特性(图2), 可用于不同材料、不同预弯曲度矫形棒对AIS矢状面平衡重建的研究。

### 1.2 不同材料矫形棒的手术模拟

采用Solidworks软件设定螺钉的材料属性, ABAQUS软件进行力学加载运算。由于CT中没有内固定材料数据, 实验采用ABAQUS软件进行模拟。上胸椎椎弓根螺钉的长度和直径为25.00 mm和



a: 前屈 b: 后伸 c: 左旋 d: 右旋  
a: Forward flexion b: Backward extension c: Left rotation d: Right rotation

图2 椎体施加载荷时的位移图

Fig. 2 Displacement diagram of vertebra under loading

3.50 mm, 胸椎中段为30.00 mm和4.00 mm, 下胸椎为40.00 mm和5.50 mm, 腰椎为45.00 mm和6.00 mm。钉棒间采用面与面接触, 相对摩擦系数为0.52。椎弓根螺钉的弹性模量与泊松比分别设定为11 000 MPa和0.3。钉棒采用四面体模拟设计, 限定置入后螺钉所有方向自由度。

矫形方式为棒平移矫形, 边界条件为约束T<sub>1</sub>椎体上部在X、Y轴方向上的自由度, 同时约束骶骨和骨盆的自由度。矫形上棒时将棒预弯一定角度, 凹侧上棒矫形。手术节段为T<sub>2</sub>~L<sub>2</sub>。上棒矫形过程中没有考虑肌肉和胸廓对手术的影响。术后测量胸椎、胸腰段和腰椎曲度, 同时测量螺钉对应的拔出力。

根据硬度不同设定矫形棒材料为钴铬合金和钛合金, 棒的直径均为6.35 mm。钛合金棒弹性模量为11 000 Mpa, 泊松比为0.30; 钴铬合金棒弹性模量为23 900 Mpa, 泊松比为0.35。分别比较2种矫形棒术后胸椎后凸、胸腰交界后凸和腰椎前凸的变化

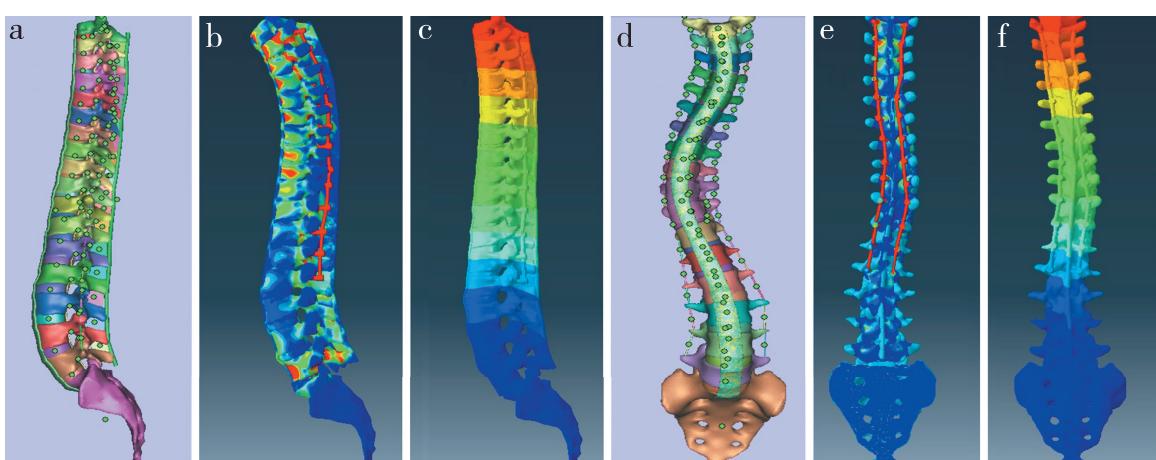
以及椎弓根螺钉拔出力。

### 1.3 不同预弯曲弧度钛合金棒手术模拟

在前述AIS模型基础上, 采用钛合金棒平移矫形。增大棒预弯弧度为40°, 比较采用不同预弯弧度(28°和40°)矫形棒对AIS矢状面力线及螺钉拔出力的影响。

## 2 结 果

当矫形棒预弯弧度为28°时, 钛合金棒矫形后胸椎后凸为12°, 胸腰段为3°, 腰椎前凸为38°; 钴铬合金棒矫形后胸椎后凸为25°, 胸腰段为3°, 腰椎前凸为38°(图3), 说明钴铬合金棒能够更好地恢复患者胸椎后凸和腰椎前凸(图4), 但使用钴铬合金棒时, 椎弓根螺钉拔出应力显著增加(图5)。当钛合金棒预弯弧度为40°时, 胸椎后凸恢复到27°, 显著优于预弯弧度为28°时, 同时螺钉拔出应力显著增加(图6~8)。



a: 术前脊柱矢状面视图 b: 钴铬合金棒矫形后脊柱矢状面位移云图 c: 钛合金棒矫形后脊柱矢状面位移云图 d: 术前脊柱冠状面视图 e: 钴铬合金棒矫形后冠状面位移云图 f: 钛合金棒矫形后位移云图

a: Sagittal plane of spine before surgery b: Cloud chart of spine in sagittal plane after surgery with cobalt-chromium alloy rod c: Cloud chart of spine in sagittal plane after surgery with titanium alloy rod d: Coronal plane of spine before surgery e: Cloud chart of spine in coronal plane after surgery with cobalt-chromium alloy rod f: Cloud chart of spine in coronal plane after surgery with titanium alloy rod

图3 不同材料矫形棒的矫形位移效果云图(预弯弧度28°)

Fig. 3 Cloud chart of orthopedic displacement of different material rods( pre-bending curve 28° )

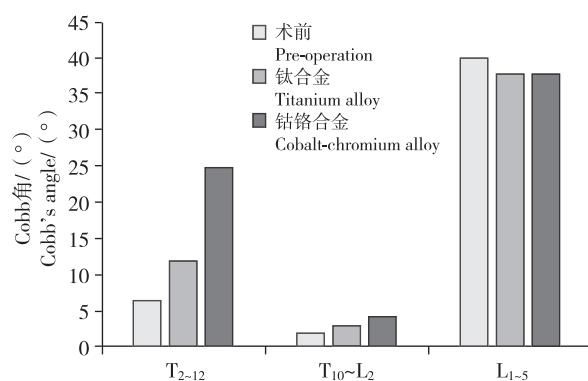


图4 矫形后胸腰椎矢状面参数的比较(预弯弧度28°)

Fig. 4 Comparison of sagittal parameters of thoracolumbar spine after orthopaedics( pre-bending curve 28° )

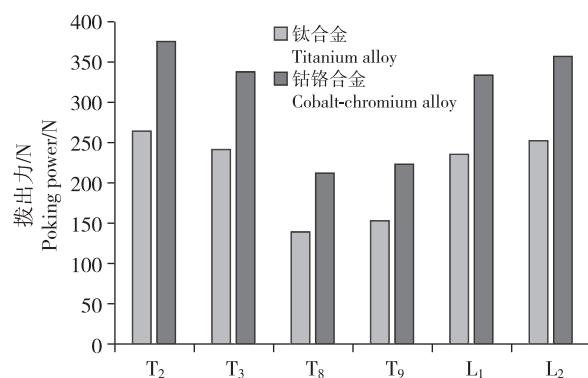
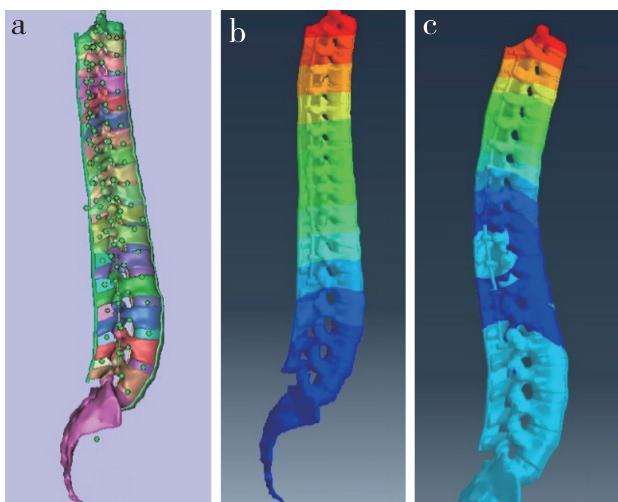


图5 螺钉在各椎体相应拔出力的比较(预弯弧度28°)

Fig. 5 Comparison of screw pullout forces at different levels( pre-bending curve 28° )



a: 术前脊柱矢状面视图 b: 预弯弧度为28°时矫形后脊柱矢状面位移云图 c: 预弯弧度为40°时矫形后脊柱矢状面位移云图  
a: Sagittal plane of spine before surgery b: Cloud chart of spine in sagittal plane after surgery with 28° pre-bending curve c: Cloud chart of spine in sagittal plane after surgery with 40° pre-bending curve

图6 不同预弯弧度钛合金棒矫形位移效果云图

Fig. 6 Cloud chart of orthopedic displacement of titanium alloy rods with different pre-bending curves

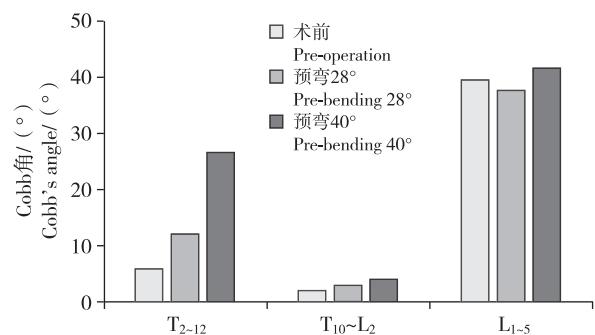


图7 使用不同预弯弧度的钛合金矫形棒术后胸腰椎矢状面参数比较

Fig. 7 Comparison of sagittal parameters between titanium alloy rods with different pre-bending curves

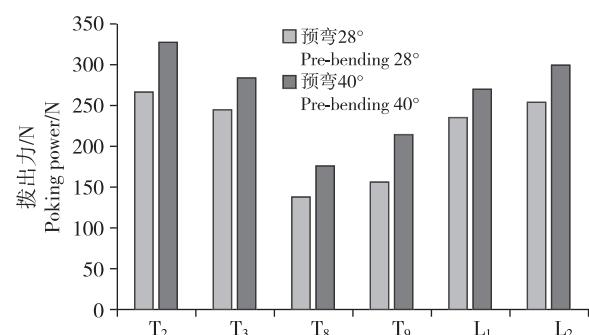


图8 使用不同预弯弧度钛合金矫形棒时螺钉在各椎体相应拔出力比较

Fig. 8 Comparison of screw pullout forces between titanium alloy rods with different pre-bending curve

### 3 讨 论

随着脊柱内固定器械的发展，全椎弓根螺钉强大的矫形力实现了 AIS 脊柱在冠状面、横断面和矢状面力线的矫正<sup>[10]</sup>。相应的手术方式也不断出现，从起初的单凹侧撑开凸侧加压到今天的截骨矫形术等<sup>[11]</sup>。有研究表明，脊柱矢状面平衡和患者生存质量具有显著相关性，恢复 AIS 患者胸腰椎生理曲度具有重要意义<sup>[12]</sup>。许多因素均可影响 AIS 术后矢状面平衡，不同材料矫形棒的矢状面重建效果不同。临床研究发现，硬度较高的钴铬合金棒能够更好地恢复患者胸椎生理曲度<sup>[13-14]</sup>，也能更好地维持冠状面和矢状面的矫形效果<sup>[7]</sup>。

本研究采用有限元模型模拟侧凸矫形手术，结果表明，矫形棒材料硬度相对较大时，胸椎后凸的重建效果更好。目前矫形棒的材料主要包括不锈钢、钛、钛合金和钴铬合金，不同材料的生物属性各异。不锈钢棒由于磁共振的兼容性差，已经很少使用。钛合金棒和钛棒具有生物力学优势，目前应用较多。钛棒钢度明显优于不锈钢棒，磁共振相容性和生物相容性好，抗疲劳性强。钴铬合金棒的刚度

比钛棒和钛合金棒都要强, 在同样的弹性回弹范围内矫形力更大, 抗疲劳性更好<sup>[15]</sup>。因此, 钴铬合金棒对于柔韧性非常差的脊柱畸形患者尤为适用。在本研究中, 矫形棒预弯弧度同样为28°时, 钴铬合金棒术后胸椎后凸恢复情况好于采用钛合金棒。既往临床研究也表明, 钴铬合金棒能够更好地重塑矢状面平衡, 同时也能够更好地维持矫形效果<sup>[7, 14]</sup>。需要注意的是, 矫形棒的刚度过大会导致棒置入节段椎体压力负荷降低, 骨钙丢失风险相对增加。既往研究报道, 内固定硬度越大, 邻近节段承受应力越大, 术后发生邻近节段退变的风险越高<sup>[16]</sup>。本研究还发现, 使用钴铬合金棒时螺钉拔出应力大于使用钛合金棒。因此, 对于上下端椎体螺钉应力较大部位, 在螺钉的选择和置入时应考虑到钴铬合金棒带来的强大剪切力和拔出力, 建议手术时适当增加螺钉数量, 并将螺钉恰当地分散在融合节段不同椎体。

本研究还发现, 术前矫形棒预弯弧度会影响AIS矢状面平衡的恢复, 适当增加矫形棒的胸段预弯弧度能够更好地维持矢状面矫形效果, 与文献报道一致<sup>[17-18]</sup>。但是当预弯弧度增加时, 也会导致螺钉拔出应力增加, 同时矫形棒的抗疲劳性会显著下降, 增加了断棒的风险<sup>[15]</sup>。目前手术医师在确定弯棒弧度时多由自身经验决定, 本研究初步探讨了采用基于金属棒性质的有限元模型预测矫形棒预弯弧度, 为个体化设计矫形棒预弯弧度及矫形棒材料选择提供了新思路。但本研究采用的是仿真模型, 无法纳入患者体质量、柔韧性、骨骼发育等情况, 其可行性仍需进一步验证。

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